

OPERATING EFFICIENCY ASSESSMENT OF COMMERCIAL BANKS WITH COOPERATIVE-STACKELBERG HYBRID TWO-STAGE DEA

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Abstract. The two-stage Data Envelopment Analysis (DEA) is widely applied to assess the efficiency of commercial banks in recent years. Even though this approach well simulates the sequence of banks production process, the independent operations within sub-stages are generally ignored, and the cooperative or non-cooperative relations between sub-stages are usually investigated separately. Commercial banking production system, however, has complex internal structure within which parallel and series structure can co-exist, and cooperative relations may concurrently occur with non-cooperative ones. In this paper, we develop a hybrid two-stage DEA to consider simultaneously the series-parallel internal structure and the cooperative-Stackelberg relations between sub-stages. The data of 19 Chinese listed commercial banks are used to show the abilities of the proposed models. This approach represents a powerful and flexible efficiency measurement implement that can be applied when the system in question has a complex internal structure in terms of both sub-systems features and sub-systems relations.

Mathematics Subject Classification. 90B30, 91-10.

Received April 21, 2021. Accepted September 26, 2021.

1. INTRODUCTION

Introduced by Charnes *et al.* [8], Data Envelopment Analysis (DEA) is a non-parametric mathematical method for assessing the relative efficiency of a set of homogenous Decision Making Units (DMUs). The banking sector is a popular field for methodological and applied researches involving DEA techniques [15]. The study of Sherman and Gold [36] is one of the first studies that apply the CCR model [8] to evaluate operating efficiency of banks. The authors point out that DEA results provide meaningful insights not available from other techniques. Over the last three decades, the banking industry has been probably becoming the most heavily studied by DEA approach of all business sectors [31].

The traditional CCR model [8] treats DMU as a black box of converting initial inputs to final outputs. Without considering the internal structure, the black box approach could not give specific information regarding the sources of inefficiency within DMUs [22], and tends to produce inaccurate efficiency scores or misleading results [16]. In classic two-stage DEA, DMU is considered as a system having two-stage internal structure, in which the initial inputs are transformed into intermediate measures [9] through the first stage, and then the intermediate measures are developed into final output in the second stage. Two-stage DEA simulates a general internal structure of the production process and provides the possibility to assess the efficiency of the whole

Keywords. Commercial bank, two-stage system, efficiency evaluation, data envelopment analysis.

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system and to decompose the overall efficiency into the efficiency of each sub-stage [10, 18, 33].

The significant applications of two-stage DEA in banking industry have been rising since the late 1990s. For example, Athanassopoulos [5] develop a two-stage DEA model to assess the operating efficiency and the quality of provided services of 68 commercial bank branches in Greece. Seiford and Zhu [34] propose a well-known two-stage DEA model that separates profitability and marketability to examine the performance of the top 55 U.S. commercial banks and indicate that the developed model is suitable to identify areas for improved bank performance over the production process. Similarly, Luo [27] evaluates the profitability and marketability performances of 245 large banks in the U.S.

The earlier studies have explicitly described the basic two-stage internal structure as deposit-producing stage and profit-earning stage linked by deposits generated from the first one. Two-stage DEA has been considerably developed in the applications to the banking efficiency measurement after 2010. Table 1 (Continued Table) summarize some of these studies.

Lozano [26] summarized more than twenty network DEA applications in the efficiency measurement of banks or bank branches, and the author indicated that most studies consider two-stage systems in series. Nevertheless, this structural feature presents certain insufficiencies in the banks performance evaluation. For example, if the operations within a sub-stage are also ordered in series, the problem can be mathematically formulated to a three-stage DEA modelling such as a network DEA framework proposed by Matthews [28] or to a more general multi-stage systems case studied by Kao [17]; but, if the internal operations of a sub-stage are organized in parallel and effectuated independently, how to evaluate and decompose the efficiency of the system with respecting the different efficiency formation mechanisms?

Indeed, there are a few studies concerning the above issues. For example, Naini *et al.* [30] consider the production process of bank as a two-stage system where the second stage includes two parallel sub-stages sharing intermediate measures. Ebrahimnejad *et al.* [12] propose a three-stage DEA model to evaluate the efficiencies of a banking system where the two first independent parallel stages are linked to the third stage. However, a common inadequacy in the two studies is that they do not offer any measures to assess the overall efficiency of system, so the overall efficiency formation mechanism is not involved in their modelling. Moreover, the relation between the deposit-producing stage and profit-earning stage is usually considered as cooperative. That is, the two stages are supposed to optimize the efficiencies simultaneously in the condition that the overall efficiency of the production system is maximized [23], and the intermediate measures are therefore to be given the same weights in both stages. However, the decision makers may prefer to give priority to one of the two stages, which will implicate potential conflicts between the two stages arising from the intermediate measures [34]. The latter situation is studied by the leader-follower or Stackelberg game EDA [24]. So, how to measure the overall efficiency and decompose it into the efficiency of each sub-system, if the cooperative and non-cooperative relations coexist in a parallel-series production system? What are the strategic implications for managers according to the cooperative situation, non-cooperative situation, and different leader-follower positions of two sub-stages?

With these questions in mind, we attempt to make up for the insufficiency of the existing two-stage DEA approaches by developing a set of cooperative-Stackelberg hybrid two-stage DEA models with consideration of complex internal structure and relations. The remainder of this paper is organized as follows. The methodology section presents the hybrid two-stage DEA models with its efficiency assessment and decomposition procedures in cooperation and cooperation-Stackelberg situations. In the illustrative application section, our proposed approach is applied to the data of 19 Chinese listed commercial banks. Section 4 outlines conclusions and future research directions.

2. METHODOLOGY

The primary task of commercial bank is to transform savings into investments and get profits as efficiently as possible. A certain sequence exists in collecting savings deposits and granting loans in the production process. Besides, the savings of commercial banks are derived mainly from household and business, and the exploitations

TABLE 1. Summary of two-stage DEA applications to the efficiency assessment of bank industry.

Authors	Models	Inputs	Intermediate measures,	Outputs
Zha and Liang [45]	Two-stage DEA with shared inputs.	Employees, Assets, Equity.	Revenues, Profits.	Market value, Earnings, Returns.
Tsolas[40]	Independent two-stage DEA.	Personnel and Rental expenses, Other operational expenses, Depreciation.	Interest and non-interest income, Loans, Commission.	Net income.
Fukuyama and Matousek [13]	Slacks-based two-stage DEA.	Labor, Capital.	Deposits.	Loans, Securities.
Ashrafi and Jaafar [4]	Two-stage DEA with undesirable input-outputs.	Personnel, Expenditures, Depreciation.	Resources.	Income, Usages, Receivable.
Avkiran and McCrystal [6]	Two-stage DEA with add. input and intermediate measures.	Capital, Labor, Customer service training.	Number of referrals, Number of transactions.	Number of referral sales.
Akther <i>et al.</i> [1]	Two-stage DEA with undesirable outputs.	Employees, Capital, Equity, Bad loans.	Deposits.	Loans, Bad loans, Investments.
Zhou <i>et al.</i> [47]	Nash bargaining two-stage DEA.	Employees, Fixed assets, Expenses.	Credit, Interbank loans.	Loans, Profits.
Wang <i>et al.</i> [42]	Additive two-stage DEA.	Labor, Fixed assets.	Deposits.	Interest income, Bad loans.
Wanke and Barros [41]	Centralized two-stage DEA.	Number of branches, Employees.	Administrative Personnel expenses.	Permanent assets, Equity.
Kwon and Lee [20]	Two-stage DEA-neural network.	Employees, Equity, Expenses.	Deposits, Loans, Investments.	Profit.
Liu <i>et al.</i> [25]	Two-stage DEA with undesirable in-inter.-output.	Employees, Fixed assets, Operating expenses.	Profits, Loans, Non-performing loans.	Market value, Earnings per share, Volatility.
Amirteimoori <i>et al.</i> [2]	Two-stage DEA with shared inputs and intermediate measures.	Fund from customers, Number of check accounts, Operating costs.	Deposits.	Number of transaction, Loans, Profits, Deposits.
Chen <i>et al.</i> [11]	Envelopment and multiplier-based two-stage DEA.	Employees, Equality.	Revenues, Profits.	Returns.
Shi <i>et al.</i> [37]	Two-stage cost efficiency DEA model.	Fixed assets, Labor and other operating expense.	Deposits.	Non-interest income, Interest income.
Fukuyama and Matousek [14]	Two-stage DEA with jointly and non-jointly good and bad outputs.	Labor, Capital.	Deposits.	Loans, non-performing loans, Securities investments.

TABLE 1. continued.

Authors	Models	Inputs	Intermediate measures,	Outputs
An <i>et al.</i> [3]	Two-stage DEA fair efficiency decomposition.	Employees, Expenses, Fixed assets.	Credits, Interbank loans.	Loans, Profits.
Kwon <i>et al.</i> [21]	BPNN approach with two-stage DEA.	Operational expenses, Equity.	Deposits.	Loans, Investments, Revenue.
Kourtzidis <i>et al.</i> [19]	Two-stage DEA with Weight Assurance model.	Employees, Total assets.	Deposits.	Loans, Securities.
Tavakoli and Mostafaee [38]	Two-stage DEA in Free Disposal Hull (FDH).	Human resources, Fixed assets, No. of branches.	Deposits.	Profits.
Mehdizadeh, <i>et al.</i> [29]	Two-stage DEA with stochastic data.	Employees, Fixed assets, Expenses.	Deposits, Interbank Deposits.	Loan, Profits.
Xu and Zhou [43]	Two-stage AR-DEA model.	Total assets, Labors, Operating expenses.	Deposits.	Interest and non-incomes, Non performing loans.
Shahbazifar, <i>et al.</i> [35]	Group efficiency of two-stage DEA.	Personnel costs, Paid interests.	Raised funds, related to currency transactions.	Loans, Common incomes.
An <i>et al.</i> [3]	Two-stage closest target DEA model.	Operation costs, Interest costs, Labors.	Deposits.	Interest income, Non-interest income.

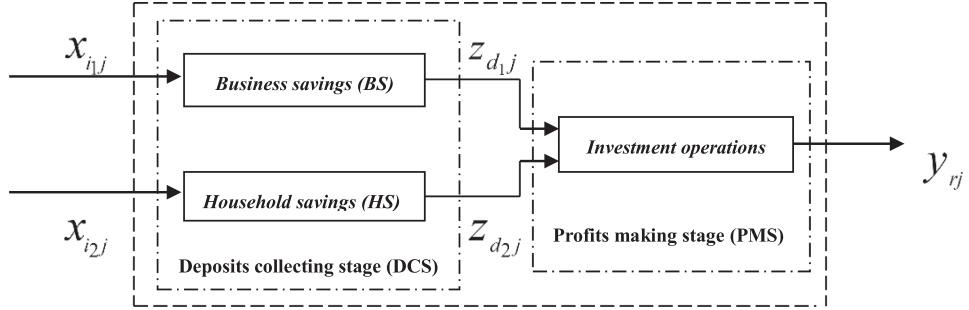


FIGURE 1. Structure of bank's hybrid two-stage production system.

of these two sources are usually conducted independently. According to these procedural characteristics, we propose to consider banking production process as a two-stage system comprised of three sub-systems as shown in Figure 1.

More specifically, we regard the commercial bank having a hybrid two-stage production system as a set of homogeneous DMUs, denoted as $DMU_j (j = 1, \dots, n)$. For any commercial bank $j, (j = 1, \dots, n)$, the deposits collecting stage (DCS) is comprised of two independent sub-systems in parallel where the business savings services system (BS) consumes I_1 operational costs $x_{i1j}, (i_1 = 1, \dots, I_1)$ to generate D_1

business deposits z_{d_1j} , ($d_1 = 1, \dots, D_1$), and the household savings services system (HS) uses I_2 operational costs x_{i_2j} , ($i_2 = 1, \dots, I_2$) to yield D_2 household deposits z_{d_2j} , ($d_2 = 1, \dots, D_2$).

The DCS is then linked to profits making stage (PMS) in series by the outputs from DCS z_{d_1j} , ($d_1 = 1, \dots, D_1$) and z_{d_2j} , ($d_2 = 1, \dots, D_2$), referred to as intermediate measures [9] or links [39]. PMS employs both household and business savings to yield S final outputs y_{rj} , ($r = 1, \dots, S$).

Let v_{i_1} and v_{i_2} denote the weights associated with the inputs x_{i_1j} , ($i_1 = 1, \dots, I_1$) and x_{i_2j} , ($i_2 = 1, \dots, I_2$), respectively. Since the intermediate measures play a dual role in DCS and PMS, we denote $u_{d_1}^1$ and $u_{d_2}^1$ as the weights on the outputs flowing from DCS, and $u_{d_1}^2$ and $u_{d_2}^2$ as the weights on the intermediate measures entering PMS, respectively. The weight u_r is given to y_{rj} , ($r = 1, \dots, S$).

2.1. Cooperative hybrid two-stage DEA approach

2.1.1. Cooperative hybrid two-stage DEA models

We start with the CCR efficiency estimation of BS and HS for DMU₀ by the following models (1) and (2), respectively.

$$\begin{aligned} \theta_0^{1.1} = \max & \frac{\sum_{d_1=1}^{D_1} u_{d_1}^1 z_{d_10}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_10}} \\ \text{s.t. } & \frac{\sum_{d_1=1}^{D_1} u_{d_1}^1 z_{d_1j}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_1j}} \leq 1, \quad j = 1, \dots, n \\ & u_{d_1}^1, v_{i_1} \geq 0, \quad d_1 = 1, \dots, D_1, \quad i_1 = 1, \dots, I_1. \end{aligned} \quad (2.1)$$

$$\begin{aligned} \theta_0^{1.2} = \max & \frac{\sum_{d_2=1}^{D_2} u_{d_2}^1 z_{d_20}}{\sum_{i_2=1}^{I_2} v_{i_2} x_{i_20}} \\ \text{s.t. } & \frac{\sum_{d_2=1}^{D_2} u_{d_2}^1 z_{d_2j}}{\sum_{i_2=1}^{I_2} v_{i_2} x_{i_2j}} \leq 1, \quad j = 1, \dots, n \\ & u_{d_2}^1, v_{i_2} \geq 0, \quad d_2 = 1, \dots, D_2, \quad i_2 = 1, \dots, I_2. \end{aligned} \quad (2.2)$$

According to the assumptions about the internal structure, BS and HS are organized in parallel and operate independently. Since there are no trade-offs between BS and HS, we propose to define the efficiency of DCS, denoted as θ_0^1 , as a weighted sum of efficiencies of BS and HS, denoted as $\theta_0^{1.1}$ and $\theta_0^{1.2}$, respectively.

$$\theta_0^1 = \max (w_1 \theta_0^{1.1} + w_2 \theta_0^{1.2}) \quad (2.3)$$

where w_1 and w_2 are the associated weights to $\theta_0^{1.1}$ and $\theta_0^{1.2}$ such that $w_1 + w_2 = 1$. In Chen *et al.* [10], these weights are specified as the proportions of total weighted resources devoted to the respective sub-systems.

$$w_1 = \frac{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_10}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} v_{i_2} x_{i_20}}, \quad \text{and} \quad w_2 = \frac{\sum_{i_2=1}^{I_2} v_{i_2} x_{i_20}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} v_{i_2} x_{i_20}}. \quad (2.4)$$

Therefore, viewed from the point of internal resources allocation, w_1 and w_2 reasonably represent the relative contribution or importance of the efficiencies of BS and HS to the performance of DCS. With models (2.1) and (2.2), and formulas (2.3) and (2.4), the efficiency of DCS can be evaluated by model (2.5):

$$\begin{aligned} \theta_0^1 = \max & \frac{\sum_{d_1=1}^{D_1} u_{d_1}^1 z_{d_10} + \sum_{d_2=1}^{D_2} u_{d_2}^1 z_{d_20}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} v_{i_2} x_{i_20}} \\ \text{s.t. } & \frac{\sum_{d_1=1}^{D_1} u_{d_1}^1 z_{d_1j}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_1j}} \leq 1, \quad j = 1, \dots, n \end{aligned}$$

$$\begin{aligned}
& \frac{\sum_{d_2=1}^{D_2} u_{d_2}^1 z_{d_2j}}{\sum_{i_2=1}^{I_2} v_{i_2} x_{i_2j}} \leq 1, \quad j = 1, \dots, n \\
& u_{d_1}^1, u_{d_2}^1, v_{i_1}, v_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
& i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2.
\end{aligned} \tag{2.5}$$

Note that the definition and procedure mentioned above are based on the thoughts of additive DEA method [10], which is developed originally to evaluate the efficiency of a two-stage system in series. However, considering that the intermediate measures are concerned in view of resources rather than its link role, it is appropriate to apply the additive method to estimate the efficiency of DCS.

The efficiency of PMS for DMU_0 , denoted as θ_0^2 , can be calculated *via* the following fractional model (2.6):

$$\begin{aligned}
\theta_0^2 = \max & \frac{\sum_{r=1}^S u_r y_{r0}}{\sum_{d_1=1}^{D_1} u_{d_1}^2 z_{d_10} + \sum_{d_2=1}^{D_2} u_{d_2}^2 z_{d_20}} \\
\text{s.t.} & \frac{\sum_{r=1}^S u_r y_{rj}}{\sum_{d_1=1}^{D_1} u_{d_1}^2 z_{d_1j} + \sum_{d_2=1}^{D_2} u_{d_2}^2 z_{d_2j}} \leq 1, \quad j = 1, \dots, n \\
& u_r, u_{d_1}^2, u_{d_2}^2 \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2.
\end{aligned} \tag{2.6}$$

Suppose that relations among all sub-systems within the production system are cooperative. That is, with given initial inputs $\sum_{i_1=1}^{I_1} v_{i_1} x_{i_1j}$ and $\sum_{i_2=1}^{I_2} v_{i_2} x_{i_2j}$, the DCS will yield optimal $\sum_{d_1=1}^{D_1} u_{d_1} z_{d_1j}$ and $\sum_{d_2=1}^{D_2} u_{d_2} z_{d_2j}$, to maximize the overall efficiency. Therefore, the weights associated with intermediate measures should be identical no matter they play the role of output from DCS or input to PMS, *i.e.*, $u_{d_1}^1 = u_{d_1}^2 = u_{d_1}$ and $u_{d_2}^1 = u_{d_2}^2 = u_{d_2}$ [18, 24]. We define then the overall efficiency, denoted as $\theta_0^{\text{overall}}$, as the product of efficiencies of DCS and PMS according to the thoughts of multiplicative DEA method [18].

$$\theta_0^{\text{overall}} = \max \theta_0^1 \cdot \theta_0^2 \tag{2.7}$$

Thus, the overall efficiency of DMU_0 can be obtained by model (2.8):

$$\begin{aligned}
\theta_0^{\text{overall}} = \max & \frac{\sum_{r=1}^S u_r y_{r0}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} v_{i_2} x_{i_20}} \\
\text{s.t.} & \frac{\sum_{d_1=1}^{D_1} u_{d_1} z_{d_1j}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_1j}} \leq 1, \quad j = 1, \dots, n \\
& \frac{\sum_{d_2=1}^{D_2} u_{d_2} z_{d_2j}}{\sum_{i_2=1}^{I_2} v_{i_2} x_{i_2j}} \leq 1, \quad j = 1, \dots, n \\
& \frac{\sum_{r=1}^S u_r y_{rj}}{\sum_{d_1=1}^{D_1} u_{d_1} z_{d_1j} + \sum_{d_2=1}^{D_2} u_{d_2} z_{d_2j}} \leq 1, \quad j = 1, \dots, n \\
& u_r, u_{d_1}, u_{d_2}, v_{i_1}, v_{i_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
& i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2.
\end{aligned} \tag{2.8}$$

By using the Charnes-Cooper transformation [7], model (2.8) can be transformed into program (9):

$$\begin{aligned}
\theta_0^{\text{overall}} = \max & \sum_{r=1}^S \mu_r y_{r0} \\
\text{s.t.} & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1j} \leq 0, \quad j = 1, \dots, n \\
& \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2j} \leq 0, \quad j = 1, \dots, n \\
& \sum_{r=1}^S \mu_r y_{rj} - \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} \leq 0, \quad j = 1, \dots, n \\
& \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_20} = 1 \\
& \mu_r, \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
& i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2.
\end{aligned} \tag{2.9}$$

The overall efficiency and the efficiencies of sub-systems can be calculated with the optimal solution to model (2.9). However, the uniqueness of optimal solution for model (2.9) is not guaranteed, and the decomposition of the overall efficiency as the product of the efficiencies of DCS and PMS should not be necessarily unique in consequence.

Moreover, it is also uncertain to obtain a uniqueness of optimal solution for model (2.5), which will make the unique efficiency decomposition for all sub-systems more complicated. As we mentioned above, sub-stages and sub-systems of the banks production system will collaborate to achieve a maximal overall efficiency in cooperative case. That is, the cooperative situation implicates that efficiency scores of sub-stage or sub-system should be at the same level whether the decision is in favour of themself or the others. In view of these, we propose a procedure of addressing the unique efficiency decomposition issues in the next sub-section.

2.1.2. Efficiency decomposition procedure

With the optimal overall efficiency obtained from model (2.9), denoted as $\theta_0^{\text{overall}*}$, we calculate either DCS efficiency θ_0^{1+} or PMS efficiency θ_0^{2+} in the most favorable manner to the stage respectively, and then derive the minimal efficiencies of the corresponding stage θ_0^{2-} or θ_0^{1-} accordingly. If $\theta_0^{1+} = \theta_0^{1-}$ or $\theta_0^{2+} = \theta_0^{2-}$, unique efficiency decomposition for DCS and PMS is achieved, *i.e.*, $\theta_0^{1+} = \theta_0^{1-} = \theta_0^{1*}$ and $\theta_0^{2+} = \theta_0^{2-} = \theta_0^{2*}$. where the “*” signifies the optimal efficiency level.

After that, we will determine either the largest efficiency score of BS $\theta_0^{1.1+}$ or that of HS $\theta_0^{1.2+}$, and derive the minimal $\theta_0^{1.2-}$ or $\theta_0^{1.1-}$ within DCS. Finally, we have unique efficiency decomposition for all stages and sub-systems if $\theta_0^{1.1+} = \theta_0^{1.1-} = \theta_0^{1.1*}$ and $\theta_0^{1.2+} = \theta_0^{1.2-} = \theta_0^{1.2*}$.

Suppose firstly that the DCS is to be given pre-emptive priority, its maximal efficiency can be calculated by solving program (10):

$$\begin{aligned}
\theta_0^{1+} = \max & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} \\
\text{s.t.} & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1j} \leq 0, \quad j = 1, \dots, n \\
& \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2j} \leq 0, \quad j = 1, \dots, n \\
& \sum_{r=1}^S \mu_r y_{rj} - \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} \leq 0, \quad j = 1, \dots, n \\
& \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_20} = 1 \\
& \sum_{r=1}^S \mu_r y_{r0} = \theta_0^{\text{overall}*} \\
& \mu_r, \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
& i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2.
\end{aligned} \tag{2.10}$$

The minimal efficiency of PMS can be then calculated as $\theta_0^{2-} = \frac{\theta_0^{\text{overall}*}}{\theta_0^{1+}}$ according to formula (2.7). Note that the efficiency of PMS θ_0^{2-} denoted with “2-” is to indicate that this stage is not given the pre-emptive priority.

Instead, the maximal efficiency of PMS can be evaluated by model (2.11), when pre-emptive priority is to be given this stage.

$$\begin{aligned}
 \theta_0^{2+} = & \max \sum_{r=1}^S \mu_r y_{r0} \\
 \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{r=1}^S \mu_r y_{rj} - \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} = 1 \\
 & \sum_{r=1}^S \mu_r y_{r0} - \theta_0^{\text{overall}*} \cdot \left(\sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_20} \right) = 0 \\
 & \mu_r, \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
 & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2.
 \end{aligned} \tag{2.11}$$

The corresponding efficiency of DCS will be $\theta_0^{1-} = \frac{\theta_0^{\text{overall}*}}{\theta_0^{2+}}$ according to formula (2.7). In other words, θ_0^{1-} is the minimal efficiency of DCS with given $\theta_0^{\text{overall}*}$ and θ_0^{2+} . As mentioned above, we have a unique efficiency decomposition for DCS and PMS if $\theta_0^{1+} = \theta_0^{1-}$ or $\theta_0^{2+} = \theta_0^{2-}$. If this is the case, we can decompose the optimal efficiency of DCS θ_0^{1*} into the efficiencies of BS and HS.

Within DCS, if BS is to be given pre-emptive priority, model (2.12) can determine its maximal efficiency $\theta_0^{1.1+}$, while maintaining the efficiency of DCS at θ_0^{1*} .

$$\begin{aligned}
 \theta_0^{1.1+} = & \max \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} \\
 \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} - \theta_0^{1*} \cdot \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_20} = \theta_0^{1*} \\
 & \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_10} = 1 \\
 & \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
 & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2.
 \end{aligned} \tag{2.12}$$

According to formula (2.3), the corresponding efficiency of HS is calculated as $\theta_0^{1.2-} = \frac{\theta_0^{1*} - w_1^* \cdot \theta_0^{1.1+}}{w_2^*}$, where w_1^* and w_2^* represent optimal weights obtained from model (2.9) by way of (4). That is, these weights guarantee the optimal efficiency of the whole system and permit BS to have a maximal efficiency. When we give pre-emptive priority to HS, its maximal efficiency can be obtained by model (2.13).

$$\begin{aligned}
 \theta_0^{1.2+} = & \max \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} \\
 \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} - \theta_0^{1*} \cdot \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_10} = \theta_0^{1*} \\
 & \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_20} = 1 \\
 & \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
 & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2.
 \end{aligned} \tag{2.13}$$

The minimal efficiency of BS can be calculated as $\theta_0^{1.1-} = \frac{\theta_0^{1*} - w_2^* \cdot \theta_0^{1.2+}}{w_1^*}$, where w_1^* and w_2^* represent optimal weights obtained from model (2.9) by way of (4). Finally, if $\theta_0^{1.1+} = \theta_0^{1.1-}$ or $\theta_0^{1.2+} = \theta_0^{1.2-}$, unique efficiency decomposition of DCS is obtained. We denote then the optimal efficiency of BS and HS as $\theta_0^{1.1*}$ and $\theta_0^{1.2*}$, respectively. With this procedure, we realize the unique efficiency decomposition of the overall efficiency of the banks production system into efficiencies of the BS, HS, and PMS, as well as that of DCS and PMS.

2.2. Cooperative-Stackelberg hybrid two-stage DEA approach

2.2.1. Non-cooperative model in deposits collecting stage leader case

Based on the thoughts of Stackelberg game or leader-follower DEA [23, 24], we develop a cooperative-Stackelberg hybrid two-stage DEA approach to evaluate and decompose the efficiency of series-parallel banking production system.

Consider again the system as illustrated in Figure 1, we suppose that there is a preference for DCS or for PMS to managers. The stage with preference is the leader stage for which the efficiency maximization is more preferable. We firstly assume that DCS is the leader. To evaluate the efficiency of the leader stage, we propose model (2.14) with reference to model (2.5).

$$\begin{aligned} \theta_0^{1(L)*} = \max & \frac{\sum_{d_1=1}^{D_1} u_{d_1} z_{d_1 0} + \sum_{d_2=1}^{D_2} u_{d_2} z_{d_2 0}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_1 0} + \sum_{i_2=1}^{I_2} v_{i_2} x_{i_2 0}} \\ \text{s.t. } & \frac{\sum_{d_1=1}^{D_1} u_{d_1} z_{d_1 j}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_1 j}} \leq 1, \quad j = 1, \dots, n \\ & \frac{\sum_{d_2=1}^{D_2} u_{d_2} z_{d_2 j}}{\sum_{i_2=1}^{I_2} v_{i_2} x_{i_2 j}} \leq 1, \quad j = 1, \dots, n \\ & u_{d_1}, u_{d_2}, v_{i_1}, v_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\ & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2. \end{aligned} \quad (2.14)$$

where “ $^{1(L)*}$ ” signifies that DCS is the leader. By using the Charnes-Cooper transformation [7], we can transform model (2.14) into model (2.15).

$$\begin{aligned} \theta_0^{1(L)*} = \max & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 0} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 0} \\ \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 0} + \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2 0} = 1 \\ & \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\ & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2. \end{aligned} \quad (2.15)$$

As the follower, PMS will maximize its efficiency by taking the DCS efficiency $\theta_0^{1(L)*}$ as a constraint. That is, the PMS will consider the optimal weights on intermediate measures $u_{d_1}^*$ and $u_{d_2}^*$ that maintain $\theta_0^1 = \theta_0^{1(L)*}$. Considering non-cooperative relations between DCS and PMS, we assume that $u_{d_1} = q \cdot \mu_{d_1}$ and $u_{d_2} = q \cdot \mu_{d_2}$. That is, the role and position of the intermediate measures are different in the two stages, but the business deposits and the household deposits are equally important to profits making activities in the second stage. We

develop then model (2.16) to evaluate the efficiency of PMS.

$$\begin{aligned}
 \theta_0^{2(S)*} = \max & \frac{\sum_{r=1}^S u_r y_{r0}}{q \left(\sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} \right)} \\
 \text{s.t. } & \frac{\sum_{r=1}^S u_r y_{rj}}{q \left(\sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} \right)} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_20} = 1 \\
 & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} = \theta_0^{1(L)*} \\
 & q, \mu_r, \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
 & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2,
 \end{aligned} \tag{2.16}$$

where “ $2(S)*$ ” signifies that PMS is the follower. Let $\mu_r = \frac{u_r}{q}$, $r = 1, \dots, S$, model (2.16) is then equivalent to model (2.17).

$$\begin{aligned}
 \theta_0^{2(S)*} = \max & \frac{\sum_{r=1}^S \mu_r y_{r0}}{\theta_0^{1(L)*}} \\
 \text{s.t. } & \sum_{r=1}^S \mu_r y_{rj} - \left(\sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} \right) \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2j} \leq 0, \quad j = 1, \dots, n \\
 & \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_20} = 1 \\
 & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} = \theta_0^{1(L)*} \\
 & \mu_r, \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\
 & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2.
 \end{aligned} \tag{2.17}$$

Note that $\theta_0^{1(L)*} \cdot \theta_0^{2(S)*} = \sum_{r=1}^S \mu_r^* y_{r0}$ at optimality with $\sum_{i_1=1}^{I_1} \nu_{i_1}^* x_{i_10} + \sum_{i_2=1}^{I_2} \nu_{i_2}^* x_{i_20} = 1$. That is, $\theta_0^{1(L)*} \cdot \theta_0^{2(S)*} = \max \frac{\sum_{r=1}^S \mu_r^* y_{r0}}{\sum_{i_1=1}^{I_1} \nu_{i_1}^* x_{i_10} + \sum_{i_2=1}^{I_2} \nu_{i_2}^* x_{i_20}}$ with the optimal solutions to model (2.17).

2.2.2. Non-cooperative model in profit making stage leader case

If we assume that PMS is the leader, the efficiency of DCS is computed subject to the requirement that the efficiency of PMS is fixed at the optimal level. We calculate the efficiency of PMS with the following standard CCR model (2.18).

$$\begin{aligned}
 \theta_0^{2(L)*} = \max & \frac{\sum_{r=1}^S u_r y_{r0}}{\sum_{d_1=1}^{D_1} u_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} u_{d_2} z_{d_20}} \\
 \text{s.t. } & \frac{\sum_{r=1}^S u_r y_{rj}}{\sum_{d_1=1}^{D_1} u_{d_1} z_{d_1j} + \sum_{d_2=1}^{D_2} u_{d_2} z_{d_2j}} \leq 1, \quad j = 1, \dots, n \\
 & u_r, u_{d_1}, u_{d_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2,
 \end{aligned} \tag{2.18}$$

where “ $2(L)*$ ” signifies that PMS is the leader. The linear model will be the following model (2.19) by using Charnes-Cooper transformation [7].

$$\begin{aligned} \theta_0^{2(L)*} &= \max \sum_{r=1}^S \mu_r y_{r0} \\ \text{s.t. } & \sum_{r=1}^S \mu_r y_{rj} - \left(\sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} \right) \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} = 1 \\ & \mu_r, \mu_{d_1}, \mu_{d_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \end{aligned} \quad (2.19)$$

when $\theta^{2(L)*}$ is obtained, the DCS efficiency can be evaluated via model (2.20).

$$\begin{aligned} \theta_0^{1(S)*} &= \max \frac{q \left(\sum_{d_1=1}^{D_1} u_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} u_{d_2} z_{d_20} \right)}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} v_{i_2} x_{i_20}} \\ \text{s.t. } & \frac{q \sum_{d_1=1}^{D_1} u_{d_1} z_{d_1j}}{\sum_{i_1=1}^{I_1} v_{i_1} x_{i_1j}} \leq 1, \quad j = 1, \dots, n \\ & \frac{q \sum_{d_2=1}^{D_2} u_{d_2} z_{d_2j}}{\sum_{i_2=1}^{I_2} v_{i_2} x_{i_2j}} \leq 1, \quad j = 1, \dots, n \\ & \sum_{r=1}^S \mu_r y_{rj} - \left(\sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} \right) \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} = 1 \\ & \sum_{r=1}^S \mu_r y_{r0} = \theta_0^{2(L)*} \\ & q, \mu_r, \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\ & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2, \end{aligned} \quad (2.20)$$

where “ $1(S)*$ ” signifies that DCS is the follower. Let $\nu_{i_1} = \frac{v_{i_1}}{q}$, $i_1 \in I_1$ and $\nu_{i_2} = \frac{v_{i_2}}{q}$, $i_2 \in I_2$, model (2.20) is then equivalent to the following linear model (2.21).

$$\begin{aligned} \frac{1}{\theta_0^{1(S)*}} &= \min \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_10} + \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_20} \\ \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{r=1}^S \mu_r y_{rj} - \left(\sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1j} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2j} \right) \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_10} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_20} = 1 \\ & \sum_{r=1}^S \mu_r y_{r0} = \theta_0^{2(L)*} \\ & \mu_r, \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad r = 1, \dots, S, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\ & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2. \end{aligned} \quad (2.21)$$

Note that from model (2.21), we have $\theta_0^{1(S)*} \cdot \theta_0^{2(L)*} = \frac{\sum_{r=1}^S \mu_r^* y_{r0}}{\sum_{i_1=1}^{I_1} v_{i_1}^* x_{i_10} + \sum_{i_2=1}^{I_2} v_{i_2}^* x_{i_20}}$ at optimality, and we observe that $\theta_0^{1(L)*} \cdot \theta_0^{2(S)*} = \frac{\sum_{r=1}^S \mu_r^* y_{r0}}{\sum_{i_1=1}^{I_1} v_{i_1}^* x_{i_10} + \sum_{i_2=1}^{I_2} v_{i_2}^* x_{i_20}}$ in model (2.17). That is, the leader-follower game DEA models imply an efficiency decomposition approach for the parallel-series system. The overall efficiency of the parallel-series banking production system is thus the product of DCS efficiency and PMS efficiency.

Note further that, $\theta_0^{1(L)*}$ and $\theta_0^{2(S)*}$ in DCS leader case, and $\theta_0^{1(S)*}$ and $\theta_0^{2(L)*}$ in PMS case, are all optimal values to linear programs. Therefore, the efficiency decomposition is unique, and the result is not affected by possible multiple optimal solutions. However, the efficiency decomposition of deposits collecting stage may not be the same in the DCS leader case and the PMS leader case.

2.2.3. Efficiency decomposition of deposits collecting stage in cooperative-Stackelberg case

Note that DCS is composed of BS and HS. We suppose that the two sub-systems operate cooperatively, or there is no priority between different sources of deposits collecting. We propose the following procedure of addressing the efficiency decomposition of the DCS.

We develop model (2.22) by reference to model (2.12) to evaluate the optimal efficiency of BS, which is to be given pre-emptive priority, while maintaining the efficiency of DCS at $\theta_0^{1(L)*}$, i.e., in the DCS leader case.

$$\begin{aligned} \theta_0^{1.1(1(L))+} &= \max \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 0} \\ \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 0} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 0} - \theta_0^{1(L)*} \cdot \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2 0} = \theta_0^{1(L)*} \\ & \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 0} = 1 \\ & \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\ & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2. \end{aligned} \quad (2.22)$$

According to formulas (2.3), the minimal efficiency of HS can be determined as $\theta_0^{1.2(1(L))-} = \frac{\theta_0^{1(L)*} - w_1^{1(L)*} \cdot \theta_0^{1.1(1(L))+}}{w_2^{1(L)*}}$, where $w_1^{1(L)*}$ and $w_2^{1(L)*}$ represent optimal weights obtained from model (2.15) by way of (2.4). These weights guarantee the optimal efficiency of DCS as leader and permit BS to have maximal efficiency.

If we give the pre-emptive priority to HS, the optimal efficiency of HS can be obtained from model (2.23).

$$\begin{aligned} \theta_0^{1.2(1(L))+} &= \max \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 0} \\ \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 0} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 0} - \theta_0^{1(L)*} \cdot \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 0} = \theta_0^{1(L)*} \\ & \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 0} = 1 \\ & \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\ & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2. \end{aligned} \quad (2.23)$$

Similarly, the corresponding minimal efficiency of BS can be calculated as $\theta_0^{1.1(1(L))-} = \frac{\theta_0^{1(L)*} - w_2^{1(L)*} \cdot \theta_0^{1.2(1(L))+}}{w_1^{1(L)*}}$, where $w_1^{1(L)*}$ and $w_2^{1(L)*}$ represent optimal weights obtained from model (2.15) by way of (2.4). If $\theta_0^{1.1(1(L))} = \theta_0^{1.1(1(L))}-$ or $\theta_0^{1.2(1(L))} = \theta_0^{1.2(1(L))}-$, unique decomposition of DCS is obtained. We denote the optimal efficiency scores of BS and HS as $\theta_0^{1.1(1(L))*}$ and $\theta_0^{1.2(1(L))*}$, respectively. With this procedure, the unique efficiency decomposition of DCS into the efficiencies of BS and HS is realized in the DCS leader case.

When PMS is the leader, we develop models (2.24) and (2.25) to calculate the efficiencies of BS and HS, with pre-emptive priority given respectively.

$$\begin{aligned} \theta_0^{1.1(2(L))+} = & \max \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 0} \\ \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 0} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 0} - \theta_0^{1(S)*} \cdot \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2 0} = \theta_0^{1(S)*} \\ & \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 0} = 1 \\ & \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\ & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2. \end{aligned} \quad (2.24)$$

$$\begin{aligned} \theta_0^{1.2(2(L))+} = & \max \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 0} \\ \text{s.t. } & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 j} - \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 j} - \sum_{i_2=1}^{I_2} \nu_{i_2} x_{i_2 j} \leq 0, \quad j = 1, \dots, n \\ & \sum_{d_1=1}^{D_1} \mu_{d_1} z_{d_1 0} + \sum_{d_2=1}^{D_2} \mu_{d_2} z_{d_2 0} - \theta_0^{1(S)*} \cdot \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 0} = \theta_0^{1(S)*} \\ & \sum_{i_1=1}^{I_1} \nu_{i_1} x_{i_1 0} = 1 \\ & \mu_{d_1}, \mu_{d_2}, \nu_{i_1}, \nu_{i_2} \geq 0, \quad d_1 = 1, \dots, D_1, \quad d_2 = 1, \dots, D_2, \\ & i_1 = 1, \dots, I_1, \quad i_2 = 1, \dots, I_2. \end{aligned} \quad (2.25)$$

According to formulas (2.3), the efficiencies of HS and BS can be determined as $\theta_0^{1.2(2(L))} = \frac{\theta_0^{1(S)*} - w_1^{1(S)*} \cdot \theta_0^{1.1(2(L))+}}{w_2^{1(S)*}}$ and $\theta_0^{1.1(2(L))} = \frac{\theta_0^{1(S)*} - w_2^{1(S)*} \cdot \theta_0^{1.2(2(L))+}}{w_1^{1(S)*}}$, respectively, where $w_1^{1(S)*}$ and $w_2^{1(S)*}$ represent optimal weights obtained from model (2.15) by way of (2.4). Finally, if $\theta_0^{1.1(2(L))} = \theta_0^{1.1(2(L))}$ or $\theta_0^{1.2(2(L))} = \theta_0^{1.2(2(L))}$, unique decomposition of DCS is obtained. We denote then the optimal efficiency scores of BS and HS as $\theta_0^{1.1(2(L))*}$ and $\theta_0^{1.2(2(L))*}$, respectively. With this procedure, the unique efficiency decomposition of DCS into the efficiencies of BS and HS is realized in the PMS leader case.

3. ILLUSTRATIVE APPLICATION

After formulating the methodological framework in the previous section, this section illustrates the proposed cooperative and cooperative-Stackelberg hybrid two-stage DEA models on the datasets of 19 main Chinese commercial banks listed in the China Stock Market.

Paradi *et al.* [32] proposed three approaches for variables selection in the banking performance evaluation: production approach, intermediary approach and profitability approach. From the viewpoint of production process, we regard the commercial bank using operational and capital costs [3, 44, 46] to produce standard outputs like incomes, profits, loans, and investment returns, *via* deposits collected from individual consumers and business consumers. The selection of input-output variable in this study is consistent with the main literature.

As illustrated in Figure 1, for any commercial bank j , ($j = 1, \dots, 19$) in the sample, the DCS is comprised by BS and HS in parallel, which uses Business banking operational costs (x_{11j}) and Business banking capital costs (x_{21j}) to generate Business deposits (z_{1j}), and uses Consumer banking operational costs (x_{12j}) and Consumer banking capital costs (x_{22j}) to generate Consumer deposits (z_{2j}), respectively. Then, PMS takes z_{1j} and z_{2j} as inputs to yield Net interest income (y_{1j}), Net commissions and fees income (y_{2j}), Net profit (y_{3j}), Earnings per share (y_{4j}), Total loans and advances (y_{5j}), and Investment returns (y_{6j}), which are considered as final outputs of the banking production system.

TABLE 2. Inputs, intermediate measures and outputs of 19 commercial banks.

Banks	x_{11}	x_{21}	x_{12}	x_{22}	z_1	z_2	y_1	y_2	y_3	y_4	y_5	y_6
BBJ	19 679	2905	3389	515	950 473	250 360	39 376	10 579	18 882	0.99	1 077 101	395
CSB	1505	53	1282	69	41 042	52 244	4997	4324	1322	0.57	77 811	107
BCD	1483	40	821	18	199 181	100 732	7463	393	3913	1.2	143 589	1694
IBCB	190 048	15 794	148 665	12 964	9 547 107	8 068 894	522 078	139 625	287 451	0.79	14 233 448	11 927
CEB	26 950	2635	21 531	1652	1 800 948	471 717	60 950	30 774	31 611	0.59	2 032 056	212
BGY	1459	284	443	85	221 114	65 917	10 861	1414	4588	1.97	7600	109
BHZ	2549	138	838	32	352 637	66 488	12 267	1617	4550	1.24	12 927	825
CCSB	166 087	5110	98 382	7974	8 430 224	7 078 489	452 456	117 798	243 651	0.96	12 903 441	6411
BJS	16 109	297	1668	243	641 999	187 693	27 815	5779	12 016	1.03	747 289	229
JRCB	669	236	118	38	37 419	36 326	2100	53	758	0.46	55 853	331
BCM	54 044	8667	40 575	18 172	3 257 639	1 541 597	127 366	40 551	70 233	0.91	4 456 914	4264
CMSB	37 278	977	33 064	735	2 446 634	523 454	86 552	47 742	50 922	1.35	2 804 307	2715
BSH	10 356	274	3449	218	651 551	205 268	19 117	6256	15 337	1.96	664 022	9637
WRCB	1496	191	204	28	37 937	28 824	2525	69	739	0.5	47 463	120
BCS	3321	475	2178	168	240 319	84 395	11 120	1094	3985	1.28	154 487	149
CMB	66 231	2930	59 968	4494	2 725 823	1 338 522	144 852	64 018	70 638	2.78	3 565 044	6205
BZZ	1272	358	472	134	168 365	67 563	8106	1865	4334	0.8	128 456	547
BOC	130 015	4266	78 168	4719	7 383 774	5 831 228	338 389	88 691	184 986	0.56	10 896 558	12 155
CCB	66 337	3309	34 067	1981	2 874 198	533 838	99 645	46 858	42 878	0.84	3 196 887	6988

TABLE 3. Overall efficiency and efficiency decomposition results of cooperative models.

Banks	$\theta_0^{\text{overall}}$	θ_0^{1+}	θ_0^{2-}	θ_0^{1-}	θ_0^{2+}	$\theta_0^{1,1+}$	$\theta_0^{1,2-}$	$\theta_0^{1,1-}$	$\theta_0^{1,2+}$	w_1^*	w_2^*
BBJ	0.3473	0.3473	1.0000	0.3473	1.0000	0.3283	0.3641	0.3283	0.3641	0.467614	0.532386
CSB	0.2862	0.2862	1.0000	0.2862	1.0000	0.2012	0.2862	0.2012	0.2862	0.000020	0.999980
BCD	0.8625	1.0000	0.8625	1.0000	0.8625	1.0000	1.0000	1.0000	1.0000	0.726298	0.273702
ICBC	0.3527	0.3527	1.0000	0.3527	1.0000	0.3561	0.3330	0.3561	0.3330	0.851342	0.148658
CEB	0.3237	0.3525	0.9183	0.3525	0.9183	0.4691	0.1400	0.4691	0.1400	0.645681	0.354319
BGY	0.9177	0.9177	1.0000	0.9177	1.0000	1.0000	0.6539	1.0000	0.6539	0.762206	0.237794
BHZ	0.7470	0.8074	0.9251	0.8074	0.9252	1.0000	0.5978	1.0000	0.5978	0.521179	0.478821
CCSB	0.3938	0.3972	0.9915	0.3972	0.9915	0.3763	0.4520	0.3763	0.4520	0.724530	0.275470
BJS	0.4912	0.4912	1.0000	0.4912	1.0000	0.4341	0.5653	0.4341	0.5653	0.565066	0.434934
JRCB	0.7319	0.8793	0.8324	0.8793	0.8324	0.3691	1.0000	0.3691	1.0000	0.191378	0.808622
BCM	0.2932	0.4060	0.7220	0.4059	0.7222	0.4064	0.1234	0.4064	0.1234	0.998750	0.001250
CMSB	0.3672	0.3680	0.9977	0.3680	0.9977	0.5029	0.1288	0.5029	0.1288	0.639421	0.360579
BSH	0.4775	0.4775	1.0000	0.4775	1.0000	0.4775	0.4019	0.4775	0.4017	0.999949	0.000051
WRCB	0.6054	0.7289	0.8306	0.7289	0.8306	0.1746	0.7289	0.1748	0.7289	0.000022	0.999978
BCS	0.3025	0.3517	0.8601	0.3517	0.8601	0.4933	0.2472	0.4933	0.2472	0.424832	0.575168
CMB	0.2531	0.2711	0.9337	0.2711	0.9337	0.3007	0.1436	0.3007	0.1436	0.811664	0.188336
BZZ	0.8002	0.8002	1.0000	0.8002	1.0000	0.8734	0.5035	0.8734	0.5035	0.802269	0.197731
BOC	0.4223	0.4474	0.9437	0.4474	0.9438	0.4201	0.5095	0.4201	0.5095	0.694451	0.305549
CCB	0.2528	0.2611	0.9683	0.2611	0.9684	0.3146	0.1080	0.3146	0.1080	0.740825	0.259175
Mean	0.4857	0.5233	0.9361	0.5233	0.9361	0.4999	0.4362	0.4999	0.4632	0.608816	0.391184

The data is derived from the 2017 annual reports of 19 Chinese listed commercial banks, including Bank of Beijing (BBJ), Changshu Bank (CSB), Bank of Chengdu (BCD), Industrial and Commercial Bank of China (ICBC), China Everbright Bank (CEB), Bank of Guiyang (BGY), Bank of Hangzhou (BHZ), China Construction Bank (CCSB), Bank of Jiangsu (BJS), Jiangsu Jiangyin Rural Commercial Bank (JRCB), Bank of Communications (BCM), China Minsheng Bank (CMSB), Bank of Shanghai (BSH), Wujiang Rural Commercial Bank (WRCB), Bank of Changsha (BCS), China Merchants Bank (CMB), Bank of Zhengzhou (BZZ), Bank of China (BOC) and China Citic Bank (CCB). Table 2 shows the data set.

We apply the developed cooperative and cooperative-Stackelberg hybrid two-stage DEA models to the dataset. The models are coded by Matlab2014a, and the results are reported in Tables 3, 4 and 5.

TABLE 4. Results of Cooperative-Stackelberg DEA model (DCS as leader).

Banks	$\theta_0^{1(L)*}$	$\theta_0^{2(S)*}$	$\theta_0^{\text{overall}(1L)*}$	$\theta_0^{1.1(1(L))+}$	$\theta_0^{1.2(1(L)) -}$	$\theta_0^{1.1(1(L)) -}$	$\theta_0^{1.2(1(L)) +}$	$w_1^{1(L)*}$	$w_2^{1(L)*}$
BBJ	0.3640	0.8842	0.3219	0.3283	0.3641	0.3283	0.3641	0.000290	0.999710
CSB	0.2862	1.0000	0.2862	0.2011	0.2862	0.2012	0.2862	0.000020	0.999980
BCD	1.0000	0.8625	0.8625	1.0000	1.0000	1.0000	1.0000	0.692946	0.307054
ICBC	0.3561	0.9358	0.3332	0.3561	0.3330	0.3561	0.3332	0.997577	0.002423
CEB	0.4690	0.5954	0.2792	0.4691	0.1400	0.4691	0.1400	0.999663	0.000337
BYG	1.0000	0.6442	0.6442	1.0000	0.6539	1.0000	0.6519	0.999990	0.000010
BHZ	1.0000	0.4276	0.4276	1.0000	0.5978	1.0000	0.6001	0.999989	0.000011
CCSB	0.4518	0.3748	0.1694	0.3763	0.4520	0.3763	0.4520	0.002240	0.997760
BJS	0.5653	0.8132	0.4597	0.4328	0.5653	0.4341	0.5653	0.000148	0.999852
JRCB	1.0000	0.6823	0.6823	0.3705	1.0000	0.3691	1.0000	0.000010	0.999990
BCM	0.4060	0.7221	0.2932	0.4064	0.1234	0.4064	0.1234	0.998750	0.001250
CMSB	0.5028	0.6465	0.3250	0.5029	0.1288	0.5029	0.1284	0.999594	0.000406
BSH	0.4775	1.0000	0.4775	0.4775	0.4017	0.4775	0.4017	0.999949	0.000051
WRCB	0.7289	0.8306	0.6054	0.1758	0.7289	0.1746	0.7289	0.000022	0.999978
BCS	0.4933	0.5148	0.2539	0.4933	0.2472	0.4933	0.2475	0.999966	0.000034
CMB	0.3005	0.8088	0.2431	0.3007	0.1436	0.3007	0.1436	0.999068	0.000932
BZZ	0.8734	0.8235	0.7192	0.8734	0.5035	0.8734	0.5042	0.999987	0.000013
BOC	0.5094	0.3418	0.1741	0.4201	0.5095	0.4201	0.5095	0.001757	0.998243
CCB	0.3145	0.6155	0.1936	0.3146	0.1080	0.3146	0.1078	0.999506	0.000494
Mean	0.5841	0.7118	0.4080	0.4999	0.4362	0.4999	0.4362	0.615341	0.384659

The second column of Table 3 reports the overall efficiency scores (Column 2) along with the efficiency decomposition results of the overall system when DCS takes priority (Columns 3 and 4), the efficiency decomposition results of the overall system when PMS takes priority (Columns 5 and 6), the efficiency decomposition results of DCS when BS is to be given pre-emptive priority (Columns 7 and 8), the efficiency decomposition results of DCS when HS is to be given pre-emptive priority (Columns 9 and 10), and the optimum weights associated with the efficiencies of BS and HS (Columns 11 and 12), respectively.

It can be seen from Table 3 that we have a unique decomposition of overall efficiency into the efficiencies of DCS and PMS for all the 19 banks. These results arise from the fact that models (2.10) and (2.11) yield identical efficiency scores for DCS or PMS whatever the priority is assigned to one of the two stages. The unique efficiency decomposition permits the cooperative hybrid two-stage DEA models to bring further to light the source of inefficiency.

We find out that the average efficiency of PMS is 0.9361, which is much higher than that of DCS (0.5233). That is to say, the commercial banks are more efficient in investment operations in general and the lower performance of DCS is probably the source of inefficiency. This result is consistent with the findings of [42] and [46], but the latters did not go deeper into the inefficient sub-stage to get more information. Therefore, it will be meaningful to move the focus of analysis to the inside of DCS. We decompose the efficiency of DCS into BS efficiency and HS efficiency. The decomposition results are reported by columns 7 to 10 in Tables 1 and 3.

It seems that BCD, BGY, and BHZ are estimated as efficient in BS, but only two banks, BCD and JRCB, are efficient in HS. The average efficiency of BS activity is slightly higher than that of HS, and we must observe with care the individual efficiency of the banks. In fact, JRCB and WRCB are both local rural commercial banks for Chinas small cities, where household savings are relatively more important than those big banks. While for the big banks, for example, ICBC, CCSB, and BOC, the efficiencies are somewhat at a similar level for the two stages.

For most banks, the efficiency of BS appears to be the driver of DCS efficiency, because the weights associated with the efficiencies of business service operations are dominant in most cases (except CSB, JRCB, WRCB). This finding is intuitive based on the importance of business banking relative to consumer banking for most commercial banks, *i.e.*, BS are generally accepted to have more influence on the performance of deposits collecting.

TABLE 5. Results of Cooperative-Stackelberg DEA model (PMS as leader).

Banks	$\theta_0^{1(S)*}$	$\theta_0^{2(L)*}$	$\theta_0^{\text{overall}(2L)*}$	$\theta_0^{1.1(2(L))+}$	$\theta_0^{1.2(2(L))-}$	$\theta_0^{1.1(2(L))-}$	$\theta_0^{1.2(2(L))+}$	$w_1^{1(L)*}$	$w_2^{1(L)*}$
BBJ	0.3473	1.0000	0.3473	0.3283	0.3641	0.3283	0.3641	0.467604	0.532396
CSB	0.2862	1.0000	0.2862	0.2011	0.2862	0.2011	0.2862	0.000001	0.999999
BCD	1.0000	0.8625	0.8625	1.0000	1.0000	1.0000	1.0000	0.726315	0.273685
ICBC	0.3527	1.0000	0.3527	0.3561	0.3330	0.3561	0.3330	0.853895	0.146105
CEB	0.3249	0.9504	0.3087	0.4691	0.1400	0.4691	0.1400	0.561716	0.438284
BGY	0.9177	1.0000	0.9177	1.0000	0.6539	1.0000	0.6539	0.762224	0.237776
BHZ	0.7360	1.0000	0.7360	1.0000	0.5978	1.0000	0.5978	0.343616	0.656384
CCSB	0.3972	0.9961	0.3938	0.3763	0.4520	0.3763	0.4520	0.724506	0.275494
BJS	0.4912	1.0000	0.4912	0.4341	0.5653	0.4341	0.5653	0.565062	0.434938
JRCB	0.5754	1.0000	0.5754	0.3690	1.0000	0.3691	0.9999	0.672934	0.327066
BCM	0.2668	1.0000	0.2668	0.4064	0.1234	0.4064	0.1234	0.506616	0.493384
CMSB	0.3666	1.0000	0.3666	0.5029	0.1288	0.5029	0.1288	0.635491	0.364509
BSH	0.4775	1.0000	0.4775	0.4775	0.4017	0.4776	0.4017	0.999999	0.000001
WRCB	0.5532	1.0000	0.5532	0.1746	0.7289	0.1746	0.7289	0.316988	0.683012
BCS	0.3154	0.9230	0.2911	0.4933	0.2472	0.4933	0.2472	0.277190	0.722810
CMB	0.2464	1.0000	0.2464	0.3007	0.1436	0.3007	0.1436	0.654142	0.345858
BZZ	0.8002	1.0000	0.8002	0.8734	0.5035	0.8734	0.5035	0.802286	0.197714
BOC	0.4474	0.9438	0.4223	0.4201	0.5095	0.4201	0.5095	0.694642	0.305358
CCB	0.2525	1.0000	0.2525	0.3146	0.1080	0.3146	0.1080	0.699178	0.300822
Mean	0.4818	0.9827	0.4710	0.4999	0.4362	0.4999	0.4362	0.592863	0.407130

However, it should be noticed that individual banks (JRCB and WRCB) having relatively low efficiency scores of the BS are evaluated with high efficiency scores of DCS. This result is not contradictive in the view of efficiency formation, because the efficiency contribution of HS is not significant in the efficiency of DCS for the two banks. Meanwhile, this result helps us to understand why a bank having inefficient sub-systems can be identified to be efficient in a particular stage even in the overall performance.

The detailed efficiency scores of sub-stage and sub-systems provide rich information about the sources of inefficiency. That is, the operation inefficiency comes from DCS for most of the commercial banks, and the efficiency of BS generally plays an important role in the efficiency formation of the DCS. Such information can help decision makers to meliorate more precisely the local or overall performance of the banking production system.

The results are obtained from our proposed cooperative approach with the assumption that none of the two stages has priority in operation efficiency maximization. Beyond these, our approach provides a set of cooperative-Stackelberg DEA models to evaluate and decompose the efficiency of the same banking production system in a non-full cooperation case. The efficiency scores are presented in Tables 4 and 5.

In Tables 4 and 5, the first three columns report the efficiency scores of DCS and PMS along with the efficiency of the overall system in the cases of DCS as the leader and PMS as the leader, respectively. The last six columns show the efficiency decomposition of DCS and the optimum weights for BS calculated by cooperative-Stackelberg DEA models. We primarily notice that there are no overall efficient banks no matter which stage is the leader.

As Tables 4 and 5 show, when DCS is the leader, the average overall efficiency is 0.4080, which is lower than that (0.4710) in PMS as leader case. The main reason given for this is that PMS is significantly more efficient when it is the leader (14 efficient banks), even if the average efficiency of DCS is lowered.

Besides, the means of overall efficiency in the cooperative-Stackelberg case with different leaders are both lower than those of overall efficiency in the cooperative approach. These results suggest that in our application, the performance of PMS is relatively dominant in the overall efficiency formation for most of the commercial banks, and non-cooperation relations between DCS and PMS will probably decrease the overall efficiency of the banking systems.

We also notice that BS and HS are carried out in parallel and undertaken independently within the DCS. This fact leads to the result that the efficiency decompositions of DCS are largely the same in the cooperative approach and in the cooperative-Stackelberg approach.

Nevertheless, testing the last two columns in Tables 4 and 5, we find out that the weights associated with the efficiencies of BS and those of HS are quietly different. The mean of the weights associated with BS efficiency is evidently greater than the mean of the weights associated with the efficiency of HS in the cooperative-Stackelberg approach. This result is consistent with that in the cooperative situation, which verifies the dominant position of business saving services in DCS for commercial banks.

Several managerial insights into the operating efficiency management of commercial banks are summarized as follows. Firstly, the source of operating inefficiency exists in DCS for most of the commercial banks, and the managers should pay more attention to improve the efficiency of this stage. Secondly, the efficiency of BS system seems to be the driver of DCS, that is to say, the BS system are relatively more important than those of HS system from the perspective of operating efficiency management.

Finally, it should be noted that, when PMS is the leader, the overall efficiency scores of the commercial banks evaluated by the cooperative-Stackelberg approach are closest to the results in the cooperative approach, which are at a relatively optimal level. This result implies that the commercial banks should prefer to a cooperative operating system, which permits to achieve the optimal overall efficiency, and they should give priority to PMS when there is conflict between DCS and PMS.

4. CONCLUSION

Based on the series structure of the banks production process, the classic two-stage DEA model has a good fit for efficiency evaluation and decomposition. But this approach has generally lost sight of the performance of parallel operations inside sub-stages, and relations between two stages are normally limited to be cooperative or competitive. The results and information issued from classic two-stage DEA models are abundant but not rich enough.

In this paper, we develop a set of cooperative and cooperative-Strackelberg hybrid two-stage DEA models to assess the operating efficiency of commercial banks. The core points of this study and the main differences of our models with those that proposed previously is that, we believe that DEA models could reveal more useful information if we go deep into the internal structure of the system, and that the relations of sub-systems would affect the efficiency performance of banks operating.

The proposed approach contributes in the following points to the efficiency evaluation and decomposition of system with complex internal structure. Firstly, we present a very general case where the series-parallel internal structure and the cooperative-Stackelberg game relations coexist in a two-stage production system. Secondly, we adopt a combination of additive and multiplicative DEA thoughts to calculate and decompose efficiencies of the system, which can portray efficiency formation mechanisms for systems with complex internal structure and relations. Thirdly, the cooperative game and the leader-follower game theories are incorporated, which can be applied in different scenarios of games between the sub-stages of the production system at once.

The application of our proposed DEA models to the datasets of 19 main Chinese commercial banks listed in the China Stock Market provides a comprehensive picture of the banks production system performance in cooperative and non-cooperative situations. The results reveal that the sources of inefficiency exist in DCS for most banks. There is no significant difference between the efficiency levels of BS and HS, but the efficiency of BS dominants the efficiency of DCS in most cases. The efficiency of PMS is significantly higher than that of DCS no matter in the cooperative situation or the cooperative-Stackelberg situation. The overall efficiency of the banking production system will achieve a relatively higher score when all the sub-systems operate cooperatively, however, non-cooperation relation between sub-stages will probably decrease the overall efficiency performance.

There are several possible future research directions that can be drawn from this study. Firstly, the proposed approach is developed under the constant returns to scale (CRS) assumption. Future work may consider how to build the models under the variable returns to scale (VRS) assumption while tanking the complex internal

structure of production system. Secondly, the undesirable outputs and uncertainty are not discussed in the proposed approach. It would be very interesting and significant to dig deeper into these aspects. Finally, the complexity of the production system can be extended to the problems of resource allocations to sub-stages within the operating system. Therefore, it becomes natural to think about how the resource allocations within the system would influence the efficiency of operating activities in the future research.

Acknowledgements. The authors wish to thank the anonymous reviewers for their constructive comments and suggestions. This work was supported by the National Natural Science Foundation of China (NSFC) under Grant 71673022.

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